FHWA-ID-EIS-12-01-F

Floodplain Technical Report

Final Environmental Impact Statement

US-95 Thorncreek Road to Moscow Project No. DHP-NH-4110(156); Key No 09294

US-95 THORNCREEK ROAD TO MOSCOW HYDRAULIC STUDY FOR AFFECTED FLOODPLAINS ON ALTERNATIVES CARRIED FORWARD

DHP-NH-4110 (156) KEY # 09294

PREPARED BY DISTRICT 2 PROJECT DEVELOPMENT ENGINEER

Curtis J. Arnzen, P.E.

03/27/15

Date

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DHP-NH-4110 (156); Key No. 9294; Thorncreek to Moscow

December 29, 2014

Preface

This report supersedes the Hydraulic Study For EIS dated April 12, 2012. The purpose of this report is to document the floodway and floodplain impacts of Alternative Modified W4 as well as the impacts of Alternatives C3 and E2. The previous report included impacts for Alternative W4 instead of Alternative Modified W4.

Introduction

This report is the Hydraulic Study for the Environmental Impact Statement for Thorncreek to Moscow. 23 CFR 650, Subpart A requires a discussion of the following items related to floodplain development:

- a. The flooding risks;
- b. The impacts on natural and beneficial floodplain values;
- c. The support of probable incompatible floodplain development;
- d. The measures to minimize floodplain impacts; and
- e. The measures to restore and preserve the natural and beneficial values.

The detail in the discussion of the items must be commensurate with the level of risk or environmental impact for the encroachment on each floodplain area. The level of detail in this Hydraulics Study is not sufficient to apply for a no rise certificate.

The Environmental Impact Statement for Thorncreek to Moscow has three action alternatives, Alternatives E2, C3, and Modified W4 and a No Action Alternative. The floodplain and floodway impacts of the alternatives are described in Table 1 shown below. The acreages have been calculated based on the most recent Flood Insurance Rate Maps (FIRM) dated August 15, 1980.

| | Table 1: Floodway and Floodplain Impacts | | | | |
|-------------|--|---------------------------|--|--|--|
| Alternative | Floodway Impacts (acre) | Floodplain Impacts (acre) | | | |
| No Action | 0.0 | 0.0 | | | |
| E2 | 0.0 | 0.0 | | | |
| C3 | 0.0 | 1.8 | | | |
| Modified W4 | 0.0 | 1.6 | | | |

DHP-NH-4110 (156); Key No. 9294; Thorncreek to Moscow

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Affected Floodplains and Floodways

No floodway impacts are anticipated in any of the action alternatives or the No Action Alternative. No floodplain impacts are anticipated on Alternative E2. Alternative Modified W4 affects 1.6 acres of total floodplain in one location labeled Site B within this report. Alternative C3 affects 1.8 acres of floodplain in 1 location labeled Site C within this report. The locations of Sites B and C are shown in Appendix A on the Floodplain Encroachment Map. District 2 personnel had two separate meetings with the Michelle Fusion, the Director of Latah County Planning and Zoning and Bill Belknap, the Community Development Director of the City of Moscow to discuss impacts to each site.

Alternative Modified W4 Site B Floodplain Impact

The 1.6 acre floodplain impact at Site B of Alternative Modified W4 is a crossing of a Zone A floodplain finger of the South Fork of the Palouse River. Zone Designation A within the FIRM is an area within a 100-year flood where base flood elevations and flood hazard factors have not been determined. The floodplain is located on farmland within the encroachment area. Michelle Fusion, the Latah County Community Development Director, indicated that Zone A floodplains generally have a low risk associated with them and that structures are usually not in close proximity to the floodplains. She said that there is "low" risk associated with this floodplain because of the low cost of property and because only a few buildings are in the vicinity of the floodplain. The buildings are all associated with Primeland Cooperatives, an agricultural cooperative.

There are no effects to natural and beneficial floodplain values since the land use is currently used as farmland. Development in this area is not anticipated at this time and the development would not be to enhance the floodplain. Steepening slopes or building retaining structures may be considered to lessen floodplain impacts if Alternative Modified W4 is selected. An oversized pipe, or pipes, would be designed to accommodate flood backwater in this location.

Since US-95 is a critical facility the proposed elevation of US-95 should be 3 feet taller than the 100 year flood elevation and a maximum of a 1 foot rise to the 100-year floodplain would be allowed.

Floodplain impacts associated with Site B are recorded in Appendix B which includes a Location Hydraulic Survey Form used by CalTrans to satisfy 23 CFR 650 for floodplain impacts on projects

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December 29, 2014

requiring Environmental Impact Statements. Appendix B also shows USGS Streamstats Data, FIRM Map copies, and photographs of Site B.

Alternative C3 Site C Floodplain Impact

The 1.8 acre floodplain impact at Site C of Alternative C3 is longitudinal Zone A floodplain encroachment of the South Fork of the Palouse River. Zone Designation A within the FIRM is an area within a 100-year flood where base flood elevations and flood hazard factors have not been determined. The floodplain encroachment is on farmland. Michelle Fusion, the Latah County Community Development Director, indicated that Zone A floodplains generally have a low risk associated with them and that structures are usually not in close proximity to the floodplains. She said that there is "low" risk associated with this floodplain because of the low cost of property and because only a few buildings are in the vicinity of the floodplain. The buildings are associated with Primeland Cooperatives, an agricultural cooperative.

There are no effects to natural and beneficial floodplain values since the land use is currently used as farmland. Development in this area is not anticipated at this time and the possible future development at this site would not enhance the floodplain. Steepening slopes or building retaining structures may be considered to lessen floodplain impacts if Alternative C3 is selected.

Since US-95 is a critical facility the proposed elevation of US-95 should be 3 feet taller than the 100 year flood elevation and a maximum of a 1 foot rise to the 100-year floodplain would be allowed.

Floodplain impacts associated with Site C are recorded in Appendix C which includes a Location Hydraulic Survey Form used by CalTrans to satisfy 23 CFR 650 for floodplain impacts on projects requiring Environmental Impact Statements. Appendix D also shows USGS Streamstats Data, FIRM Map copies, and photographs of Site C.

Recent Floodplain Investigation of South Fork of Palouse River

ITD D2 Personnel had a meeting with Bill Belknap, the Community Development Director of Moscow. He indicated that a local civil engineering firm named Terra Graphics completed an extensive floodplain and floodway investigation near Sites B and C for a proposed industrial park in Southeast Moscow that may affect the floodplain and floodway areas at Sites B and C if

the analysis is approved by FEMA. Terra Graphics indicated in Memorandum #4 – Southeast Moscow Industrial Park Existing Condition Hydraulic Model, dated February 22, 2010, that they updated the HEC-2 hydraulic model used to create the August 15, 1980 FIRM Maps in order to define a new 100-year flood elevation with more accurate survey data and the preferred HEC-RAS hydraulic model. The results of this model are that the 100 year flood elevation decreases and that Sites B and C impacts would no longer be in a 100-year floodplain. If Terra Graphics's calculations used to create Memorandum #4, shown in Appendix E, are correct and approved by FEMA, Sites B and C will not be a floodplain impact on Alternatives C3 and Modified W4.

Conclusion

Floodplain and floodway impacts are shown in Table 2 below:

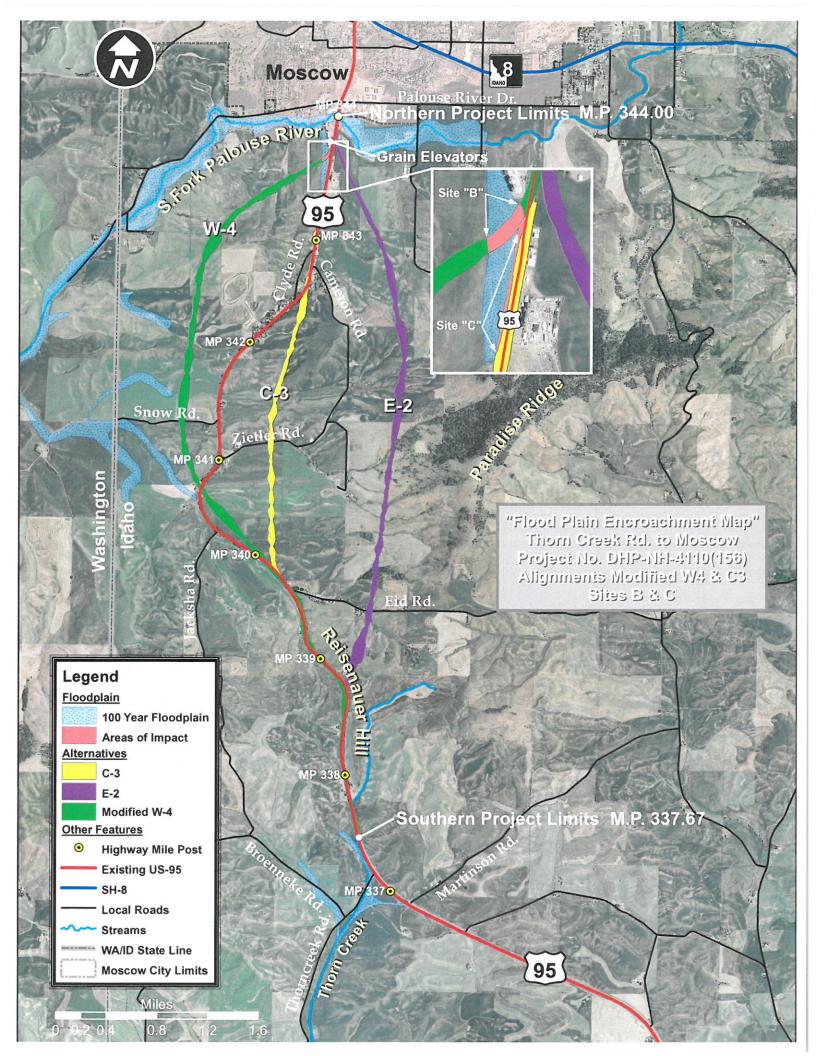
| Table 2: Floodway and Floodplain Impacts | | | | |
|--|-------------------------|---------------------------|--|--|
| Alternative | Floodway Impacts (acre) | Floodplain Impacts (acre) | | |
| No Action | 0.0 | 0.0 | | |
| E2 | 0.0 | 0.0 | | |
| C3 | 0.0 | 1.8 | | |
| Modified W4 | 0.0 | 1.6 | | |

There are no floodway impacts for Alternatives E2, C3, and Modified W4 and for the No Action Alternative and there are no floodplain impacts for the No Action Alternative and Alternative E2.

Alternative Modified W4 has 1.6 total acres of floodplain impacts in one location at Site B which is a crossing of a finger of floodplain used for the South Fork of the Palouse River that is currently used as farm field at the north end of the project. The floodplain is in Zone A of the FIRM maps and has no natural or beneficial floodplain value. Filling into the floodplains at Site B on Alternative Modified W4 has a low associated risk for future flooding potential.

C3 has 1.8 total acres of floodplain impacts in one location (Site C). The floodplain impact area is a longitudinal encroachment of a finger of floodplain of the South Fork of the Palouse River that is currently used as farm field at the north end of the project. The floodplains are in Zone A of the FIRM maps and have no natural or beneficial floodplain value. Filling into the floodplain at Site C on Alternative C3 has a low associated risk for future flooding potential.

Appendix A Floodplain Encroachment Map



Appendix B Site B Information

EIS Hydraulics Study Form for Site B

USGS Stream Stats Data for Site B

Federal Insurance Rate Map for Site B

Photos of Site B

LOCATION HYDRAULIC STUDY FORM THORN CREEK ROAD TO MOSCOW PROJECT NO. DHP-NH-4110(156) ALIGNMENT- MODIFIED W4 SITE B

District 02 County Latah Route US-95 Mile Post 343.475

Floodplain Description:

This floodplain is a finger of the Southfork of the Palouse River outside the southern City Limits of Moscow. The FIRM panels show that it is classified as a Zone A floodplain with no 100-year flood elevation being determined by FEMA. The floodplain is currently used as an agricultural field and no buildings are within the floodplain, but buildings associated with Primeland Cooperatives are in close proximity. The proposed location crossing the floodplain is approximately at Latitude 46.710160°, Longitude - 117.0050003° just South of Moscow, Idaho.

See the Latah County, Idaho Flood Insurance Rate Map, Panel 160086 0330D, Section 19, Township 39 North, Range 5 West, Boise Meridian.

1. Description of Proposal

A proposed 4 lane roadway with a divided median would cross the floodplain finger and divide it impacting about 1.6 total acres. The impact could be minimized by slope adjustment or retaining walls. Drainage culverts sized to accommodate backwater of a 100 year flood event the South Fork of the Palouse River would be added through the highway embankment. If this alignment was chosen we would fill out a Floodplain Development Application for Latah County Planning and Zoning to meet their requirements. The floodplain could not rise more than 1 foot and the elevation of the roadway would need to be 3 feet taller than the 100 year flood elevation. Latah County Planning and Zoning indicated that this encroachment was minimal and that there is low associated risk with filling in this floodplain.

| associated III | on with hims in the | поочрши | | | |
|---------------------|--|--------------------|---|----------------------------------|----------------|
| 2. ADT: | Current 6400 | Projected 10 | 0221 | | |
| The f | Data: Base Flood lood of record, if great topping flood Q=NA | eater than Q100: N | $ \underline{\mathbf{ft}^{3}} / \mathbf{s} \mathbf{WS} $ $ \mathbf{NA} \mathbf{Q} = \underline{\mathbf{N}} $ $ \mathbf{WSE} = \underline{\mathbf{NA}} $ | \mathbf{A} ft ³ / s | WSE= <u>NA</u> |
| which is attached | on calculations from the Str l. face elevation was determi | | | | |
| Are N | NFIP maps and studi | es available? | YES_XX | | NO |
| 4. Is the high YES_ | way location alterna | | ulatory flood | way ? | |

| 5. Attach map with flood limits outlined showing all buildings or other improvements within the base floodplain. | | | | | |
|--|--|--|--|--|--|
| No buildings are within the floodplain, but buildings associated with Primland Cooperatives are close to the floodplain. | | | | | |
| Potential Q100 backwater damages: | | | | | |
| A. Residences? NO XX YES B. Other Bldgs? NO XX YES C. Crops? NO YES XX D. Natural and beneficial Floodplain values? NO XX YES | | | | | |
| 6. Type of Traffic: | | | | | |
| A. Emergency supply or evacuation route? NOYESXX_ B. Emergency vehicle access? NOYESXX_ C. Practicable detour available? NOYESXX_ D. School bus or mail route? NOYESXX_ 7. Estimated duration of traffic interruption for 100-year event hours: No Interruption 8. Estimated value of Q100 flood damages (if any) – moderate risk level. A. Roadway \$N/A B Property \$N/A Total \$N/A Total \$N/A | | | | | |
| 9. Assessment of Level of Risk Low_XX_ Moderate High | | | | | |
| For High Risk projects, during design phase, additional Design Study Risk Analysis May be necessary to determine design alternative. | | | | | |
| Is there any longitudinal encroachment, significant encroachment, or any support of incompatible Floodplain development? NO_XX_YES | | | | | |
| If yes, provide evaluation and discussion of practicability of alternatives in accordance with 23 CFR 650.113 | | | | | |

Information developed to comply with the Federal requirement for the Location Hydraulic Study shall be retained in the project files.

Signature – D2PDE $\frac{2}{2}$ Date $\frac{3}{2}$



Basin Characteristics Report

Date: Thu Mar 29 2012 08:41:58 Mountain Daylight Time NAD27 Latitude: 46.7134 (46 42 48) NAD27 Longitude: -117.0064 (-117 00 23) NAD83 Latitude: 46.7132 (46 42 48) NAD83 Longitude: -117.0074 (-117 00 27)

| Parameter | Value |
|--|-------|
| Area that drains to a point on a stream, in square miles | 28.05 |
| Mean annual precipitation, in inches | 24.4 |
| Minimum Basin Elevation in feet | 2540 |
| Maximum Basin Elevation in feet | 4990 |
| Mean Basin Elevation in feet | 2970 |
| Maximum - minimum elevation, in feet | 2450 |
| Mean basin slope computed from 10 m DEM, in percent | 18 |
| Mean basin slope. Computed from 10 m DEM and adjusted to approximate earlier values computed from 30 m DEM. | 16.4 |
| Percent of area having slope greater than or equal to 30 percent, computed from 10-m DEM | 16 |
| Percent of area with slopes greater than 30 percent. Computed from 10 m DEM and adjusted to approximate earlier values based on 30-m DEMs | 12.3 |
| Percentage of area having slopes greater than 50 percent, computed from 30-meter DEMs | 0.68 |
| Percent of area having North-facing slopes greater than or equal to 30 percent, computed from 10-m DEM | 4 |
| Percent of area having North-facing slopes greater than or equal to 30 percent. Computed from 10 m DEM and adjusted to approximate values computed from 30 m DEM | . 3 |
| 10-85 slope based on longest flow path computed using 10-m DEMs, in feet per mile | 75.2 |
| 10-85 slope, in feet per mile. Computed based on longest flow path using 10-m DEMs and adjusted to approximate earlier measurements done using BASINSOFT. | 75.9 |
| Percent of drainage area as surficial volcanic rocks as defined in SIR 2006-5035 | 66.7 |
| Percent of area covered by forest | 23 |
| Agricultural Land in Percentage of Drainage Area | 65.4 |
| Developed Land In Percentage of Drainage Area from 1992 NLCD data | 2.76 |
| Percentage of area covered by water or perennial ice or snow from NLCD1992 | 0.12 |
| Percentage of impervious area determined from NLCD 2001 impervious dataset | 0.99 |
| Percentage of urban land cover determined from NLCD 2001 land cover dataset | 5.37 |

Streamstats Ungaged Site Report

Date: Thu Mar 29 2012 08:47:26 Mountain Daylight Time

Site Location: Idaho

NAD27 Latitude: 46.7134 (46 42 48)
NAD27 Longitude: -117.0064 (-117 00 23)
NAD83 Latitude: 46.7132 (46 42 48)
NAD83 Longitude: -117.0074 (-117 00 27)

Drainage Area: 28.05 mi2 Percent Urban: 5.38 % Percent Impervious: 0.99 %

| 100% Peak Flow Region 3 | (28.1 m | i2) | |
|------------------------------|---------|---------------------------------|--------|
| Parameter | Value | Regression Equation Valid Range | |
| Parameter | | Min | Max |
| Drainage Area (square miles) | 28.1 | 2 | 788.7 |
| Mean Basin Elevation (feet) | 2970 | 1458.4 | 4040.1 |

| 100% Low Flow Region 3 (28.1 | Value | Regression Equatio | n Valid Bango |
|------------------------------------|-------|--------------------|---------------|
| Parameter | Value | Min | Max |
| Drainage Area (square miles) | 28.1 | 17.6 | 674.9 |
| Mean Basin Elevation (feet) | 2970 | 2647.1 | 3752.2 |
| Mean Annual Precipitation (inches) | 24.4 | 19.3 | 30.1 |
| Relief (feet) | 2450 | 1442.8 | 5098.9 |

Zero-Flow Probability Basin Characteristics 100% Undefined Region (28.05 mi2)

The selected watershed is entirely in an area for which flow equations were not defined.

| 100% Low Flow Region 3 (28.1 | mi2) | | | |
|------------------------------------|-------|---------------------------------|--------|--|
| Parameter | Value | Regression Equation Valid Range | | |
| rarameter | | Min | Max | |
| Drainage Area (square miles) | 28.1 | 17.6 | 674.9 | |
| Mean Basin Elevation (feet) | 2970 | 2647.1 | 3752.2 | |
| Mean Annual Precipitation (inches) | 24.4 | 19.3 | 30.1 | |
| Relief (feet) | 2450 | 1442.8 | 5098.9 | |

| | | | Equivalent years of record | 90-Percent Prediction Interva | | |
|-----------|---------------------------|----------------------------|----------------------------------|-------------------------------|---------|--|
| Statistic | Flow (ft ³ /s) | Prediction Error (percent) | | Minimum | Maximum | |
| PK1_5 | 198 | 84 | | 57.2 | 686 | |
| PK2 | 271 | 69 | | 94.2 | 782 | |
| PK2_33 | 310 | 63 | | 116 | 826 | |
| PK5 | 505 | 49 | | 229 | 1120 | |
| PK10 | 693 | 44 | | 336 | 1430 | |
| PK25 | 970 | 43 | | 476 | 1980 | |
| PK50 | 1200 | 44 | | 575 | 2490 | |
| PK100 | 1440 | 46 | | 665 | 3100 | |
| PK200 | 1690 | 49 | | 746 | 3840 | |
| PK500 | 2060 | 54 | | 845 | 5020 | |

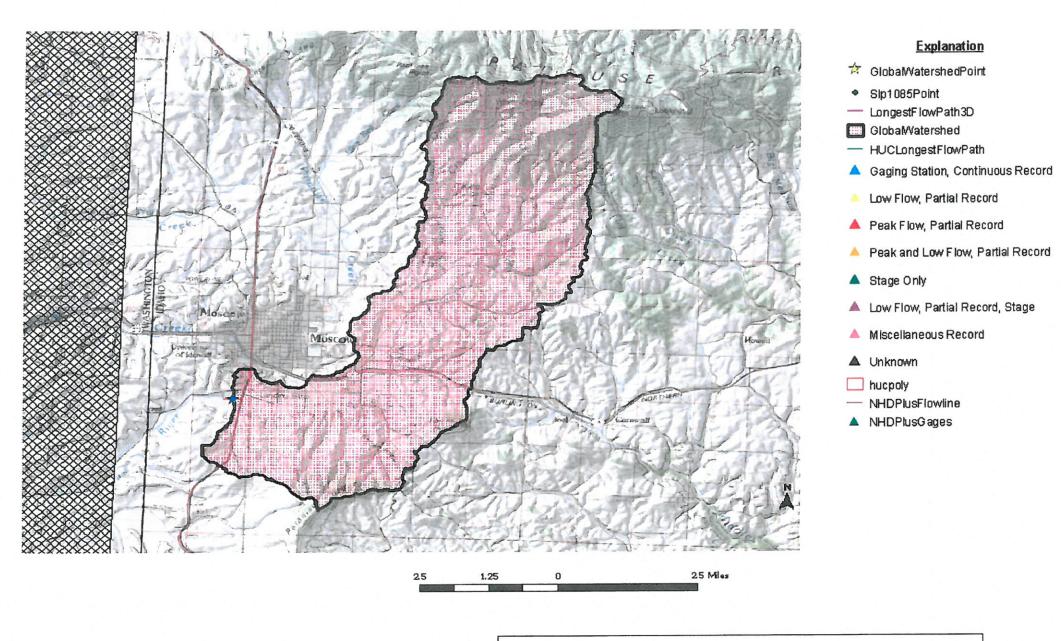
| | | | Equivalent | 90-Percent Prediction Interva | |
|-----------|---------------------------|----------------------------|--------------------|-------------------------------|---------|
| Statistic | Flow (ft ³ /s) | Estimation Error (percent) | years of record | Minimum | Maximum |
| M1D10Y | 0.36 | 130 | | | |
| M7D10Y | 0.5 | 130 | | | |

| M7D2Y | 0.71 | 75 | |
|--------|------|----|--|
| M30D5Y | 0.84 | 83 | |

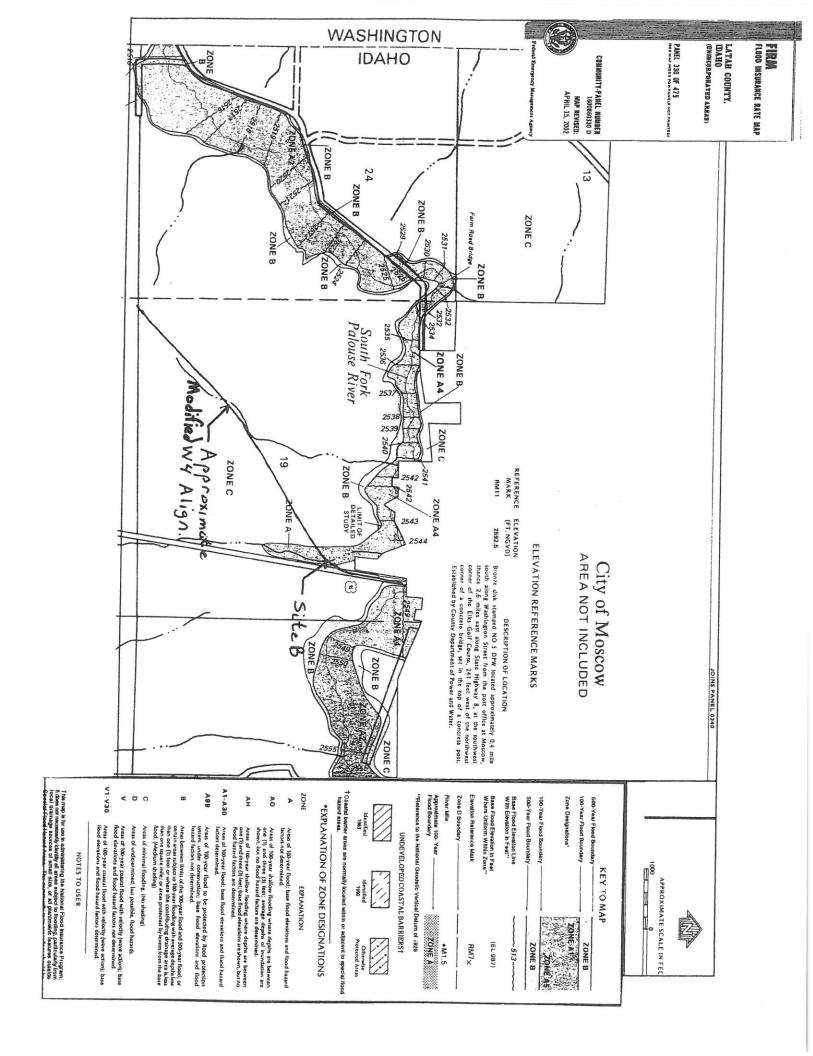
| Monthi | y and Anni | ual Streamflow Statisti | cs | | | |
|-----------|---------------------------|----------------------------|---------------------|---------------|------------------|--|
| Chatietic | FI (03/-) | Estimation Empr (sausset) | Equivalent years of | 90-Percent Pr | ediction Interva | |
| Statistic | Flow (ft ² /s) | Estimation Error (percent) | record | Minimum | Maximum | |
| QA | 10.8 | 17 | | | | |
| JAND20 | 21.3 | 46 | | | | |
| JAND50 | 6.65 | 43 | | | | |
| JAND80 | 2.05 | 21 | | | | |
| FEBD20 | 39.5 | 39 | | | | |
| FEBD50 | 14.5 | 19 | | | | |
| FEBD80 | 5.02 | 27 | | | | |
| MARD20 | 40.5 | 41 | | | | |
| MARD50 | 19.3 | 26 | | | | |
| MARD80 | 6.9 | 26 | | | | |
| APRD20 | 19.2 | 44 | | | | |
| APRD50 | 8.74 | 46 | | | | |
| APRD80 | 4.18 | 62 | | | | |
| MAYD20 | 8.3 | 61 | | | | |
| MAYD50 | 3.85 | 51 | | | | |
| MAYD80 | 2.37 | 44 | | | | |
| JUND20 | 4.01 | 43 | | | | |
| JUND50 | 2.55 | 30 | | | | |
| JUND80 | 1.89 | 36 | | | | |
| JULD20 | 2.06 | 21 | | | | |
| JULD50 | 1.83 | 30 | | | | |
| JULD80 | 1.73 | 50 | | | | |
| AUGD20 | 1.84 | 28 | | | | |
| AUGD50 | 1.78 | 44 | | | | |
| AUGD80 | 1.73 | 96 | | | | |
| SEPD20 | 1.88 | 22 | | | | |
| SEPD50 | 1.78 | 33 | | | | |
| SEPD80 | 1.72 | 63 | | | | |
| OCTD20 | 1.94 | 26 | | | | |
| OCTD50 | 1.83 | 25 | | | | |
| OCTD80 | 1.73 | 37 | | | | |
| NOVD20 | 3.21 | 67 | | | | |
| NOVD50 | 1.8 | 29 | | | | |
| NOVD80 | 1.77 | 28 | | | | |
| DECD20 | 7.26 | 49 | | | | |
| DECD50 | 1.85 | 42 | | | | |
| DECD80 | 1.81 | 22 | i | | | |

StreamStats Print Page

SO. FORK PALOUSE RV.



3/29/2012 8:26:34 AM



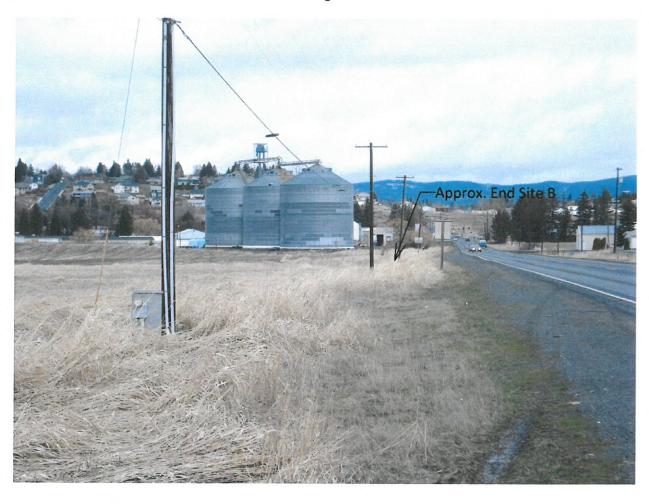
PROJECT NO. DHP-NH-4110(156) FLOOD PLAIN PHOTOS ALIGNMENT MODIFIED W-4 SITE B

Approximate Beginning of Crossing of Flood Plain Encroachment at Site B Looking North



Approximate End of Crossing of Flood Plain Encroachment at Site B

Looking North



Appendix C Site C Information

EIS Hydraulics Study Form for Site C
USGS Stream Stats Data for Site C
Federal Insurance Rate Map for Site C
Photos of Site C

LOCATION HYDRAULIC STUDY FORM THORN CREEK ROAD TO MOSCOW **PROJECT NO. DHP-NH-4110(156) ALIGNMENT- C-3** SITE C

District 02 County Latah Route US-95 Mile Post 343.457 to Mile Post 343.651

Floodplain Description:

This floodplain is a finger of the Southfork of the Palouse River outside the southern City Limits of Moscow. The FIRM panels show that it is classified as a Zone A floodplain with no 100-year flood elevation being determined by FEMA. The floodplain is currently used as an agricultural field and no buildings are within the floodplain, but buildings associated with Primeland Cooperatives are in close proximity. The proposed encroachment location is approximately starting at Latitude 46.705919°, Longitude -117.005757° to Latitude 46.7089546°, Longitude -117.0050693° just South of Moscow, Idaho. See the Latah County, Idaho Flood Insurance Rate Map, Panel 160086 0330D, Section 19, Township 39 North, Range 5 West, Boise Meridian.

1. Description of Proposal

A proposed 4 lane roadway with a divided median would create a longitudinal encroachment on the floodplain finger that is about 2.0 acres in size. Effects to the floodplain could be minimized by slope adjustment or retaining walls. If this alignment was chosen, a Floodplain Development Application for Latah County Planning and Zoning to meet their requirements would be completed. The floodplain could not rise more than 1 foot and the elevation of the roadway would need to be 3 feet taller than the 100 year flood elevation. Latah County Planning and Zoning indicated that this encroachment was minimal and that there is low associated risk with filling in this floodplain.

10221

| 2. ADT: | Curre | nt <u>6400</u> | -: | Project | ted | 10221 | _ | |
|-----------------------|----------|---|-----------------|--|-------------------------------|------------------|------|--|
| 3. Hydraulic The i | flood of | Base Flood Q ₁ record, if greater flood Q= NA ft ³ | than Q100: NA | $_{\text{ft}^3}$ / s $_{\text{Q}}$ Q= $_{\text{NA}}$ $_{\text{WSE}}$ = | 1 _ft ³ / s | 00= ** S WSE= | = NA | |
| which is attached | d. | ions from the Stream . ion was determined o | | | | | | |
| Are l | NFIP ma | ps and studies av | vailable? | YES_ | XX | _ | NO | |
| 4. Is the high YES | nway loc | ation alternative NO | within a regula | atory flo | oodway | ? | | |

| 5. Attach map with flood limits outlined showing all buildings or other improvements within the base floodplain. |
|--|
| No buildings are within the floodplain, but buildings associated with Primland Cooperatives are close to the floodplain. |
| Potential Q100 backwater damages: |
| A. Residences? NO XX YES B. Other Bldgs? NO XX YES C. Crops? NO YES XX D. Natural and beneficial Floodplain values? NO XX YES |
| 6. Type of Traffic: |
| A. Emergency supply or evacuation route? NO YES XX B. Emergency vehicle access? NO YES XX C. Practicable detour available? NO YES XX D. School bus or mail route? NO YES XX |
| 7. Estimated duration of traffic interruption for 100-year event hours: No Interruption |
| 8. Estimated value of Q100 flood damages (if any) – moderate risk level. |
| A. Roadway \$N/A B Property \$N/A Total \$N/A |
| 9. Assessment of Level of Risk Low_XX Moderate High |
| For High Risk projects, during design phase, additional Design Study Risk Analysis May be necessary to determine design alternative. |
| Is there any longitudinal encroachment, significant encroachment, or any support of incompatible Floodplain development? NO_XX_YES |
| If yes, provide evaluation and discussion of practicability of alternatives in accordance with 23 CFR 650.113 |
| Information developed to comply with the Federal requirement for the Location Hydraulic Study shall be retained in the project files. |
| Signature – D2PDE Cuty Cury Date 4//2//2 |



Basin Characteristics Report

Date: Thu Mar 29 2012 08:41:58 Mountain Daylight Time NAD27 Latitude: 46.7134 (46 42 48) NAD27 Longitude: -117.0064 (-117 00 23) NAD83 Latitude: 46.7132 (46 42 48) NAD83 Longitude: -117.0074 (-117 00 27)

| Parameter | Valu |
|---|------|
| Area that drains to a point on a stream, in square miles | 28. |
| Mean annual precipitation, in inches | 24 |
| Minimum Basin Elevation in feet | 254 |
| Maximum Basin Elevation in feet | 499 |
| Mean Basin Elevation in feet | 297 |
| Maximum - minimum elevation, in feet | 245 |
| Mean basin slope computed from 10 m DEM, in percent | 1 |
| Mean basin slope. Computed from 10 m DEM and adjusted to approximate earlier values computed from 30 m DEM. | 16. |
| Percent of area having slope greater than or equal to 30 percent, computed from 10-m DEM | 1 |
| Percent of area with slopes greater than 30 percent. Computed from 10 m DEM and adjusted to approximate earlier values based on 30-m DEMs | 12. |
| Percentage of area having slopes greater than 50 percent, computed from 30-meter DEMs | 0.6 |
| Percent of area having North-facing slopes greater than or equal to 30 percent, computed from 10-m DEM | i . |
| Percent of area having North-facing slopes greater than or equal to 30 percent. Computed from 10 m DEM and adjusted to approximate values computed from 30 m DEM. | |
| 10-85 slope based on longest flow path computed using 10-m DEMs, in feet per mile | 75.2 |
| 10-85 slope, in feet per mile. Computed based on longest flow path using 10-m DEMs and adjusted to approximate earlier measurements done using BASINSOFT. | 75.9 |
| Percent of drainage area as surficial volcanic rocks as defined in SIR 2006-5035 | 66.7 |
| Percent of area covered by forest | 23 |
| gricultural Land in Percentage of Drainage Area | 65.4 |
| Developed Land in Percentage of Drainage Area from 1992 NLCD data | 2.76 |
| ercentage of area covered by water or perennial ice or snow from NLCD1992 | 0.12 |
| ercentage of impervious area determined from NLCD 2001 impervious dataset | 0.99 |
| ercentage of urban land cover determined from NLCD 2001 land cover dataset | 5.37 |

Streamstats Ungaged Site Report

Date: Thu Mar 29 2012 08:47:26 Mountain Daylight Time Site Location: Idaho
NAD27 Latitude: 46.7134 (46 42 48)
NAD27 Longitude: -117.0064 (-117 00 23)
NAD83 Latitude: 46.7132 (46 42 48)
NAD83 Longitude: -117.0074 (-117 00 27)
Drainage Area: 28.05 mi2
Percent Urbanis -5.38 %
Percent Urbanious: 0.98 %

Percent Impervious: 0.99 %

| 100% Peak Flow Region 3 | (28.1 m | i2) | |
|------------------------------|---------|---------------------|----------------|
| Parameter | Value | Regression Equation | on Valid Range |
| | | Min | Max |
| Drainage Area (square miles) | 28.1 | 2 | 788.7 |
| Mean Basin Elevation (feet) | 2970 | 1458.4 | 4040. |

| Low-Flow Basin Character | | | |
|------------------------------------|-------|--------------------|---------------|
| 100% Low Flow Region 3 (28.1 | Value | Regression Equatio | n Valid Range |
| Parameter | | Min | Max |
| Drainage Area (square miles) | 28.1 | 17.6 | 674.9 |
| Mean Basin Elevation (feet) | 2970 | 2647.1 | 3752.2 |
| Mean Annual Precipitation (Inches) | 24.4 | 19.3 | 30.1 |
| Relief (feet) | 2450 | 1442.8 | 5098.9 |

Zero-Flow Probability Basin Characteristics 100% Undefined Region (28.05 mi2)

The selected watershed is entirely in an area for which flow equations were not defined.

| 100% Low Flow Region 3 (28.1 | mi2) | | |
|------------------------------------|-------|---------------------|---------------|
| Parameter | Value | Regression Equation | n Valid Range |
| 7 di dilictei | | Min | Max |
| Drainage Area (square miles) | 28.1 | 17.6 | 674.9 |
| Mean Basin Elevation (feet) | 2970 | 2647.1 | 3752.2 |
| Mean Annual Precipitation (inches) | 24.4 | 19.3 | 30.1 |
| Relief (feet) | 2450 | 1442.8 | 5098.9 |

| Sanai-ai-lin | | | Equivalent | 90-Percent Prediction Interva | | |
|--------------|---------------------------|----------------------------|--------------------|-------------------------------|---------|--|
| Statistic | Flow (ft ² /s) | Prediction Error (percent) | years of record | Minimum | Maximum | |
| PK1_5 | 198 | 84 | | 57.2 | 686 | |
| PK2 | 271 | 69 | | 94.2 | 782 | |
| PK2_33 | 310 | 63 | | 116 | 826 | |
| PK5 | 505 | 49 | | 229 | 1120 | |
| PK10 | 693 | 44 | | 336 | 1430 | |
| PK25 | 970 | 43 | | 476 | 1980 | |
| PK50 | 1200 | 44 | | 575 | 2490 | |
| PK100 | 1440 | 46 | | 665 | 3100 | |
| PK200 | 1690 | 49 | | 746 | 3840 | |
| PK500 | 2060 | 54 | | 845 | 5020 | |

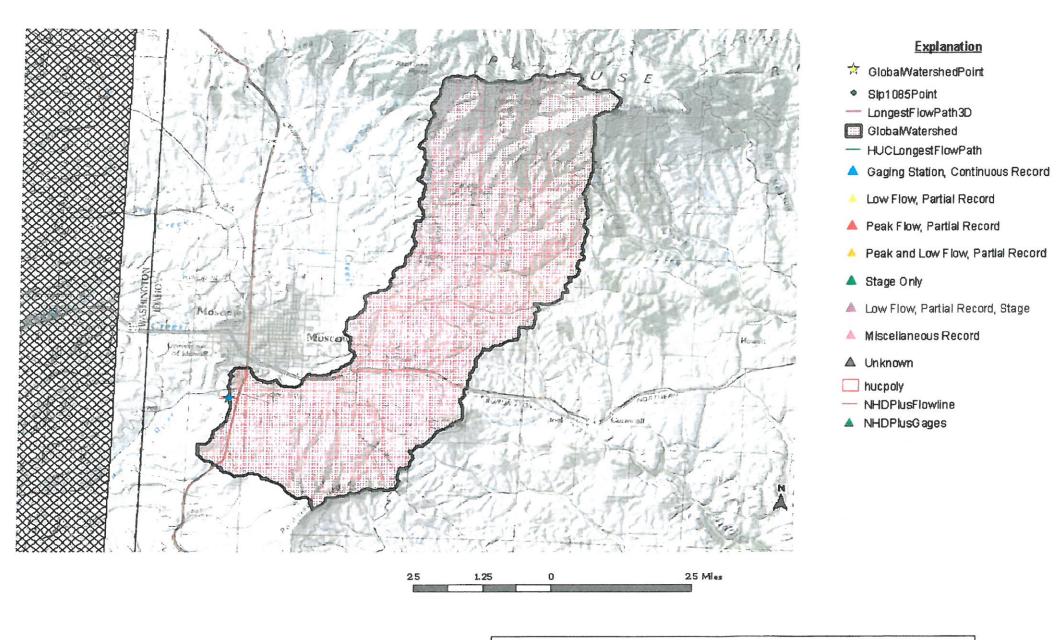
| Statistic Flow (ft ³ /s) | | | Equivalent | 90-Percent Prediction Interva | | |
|-------------------------------------|----------------------------|--------------------|------------|-------------------------------|--|--|
| | Estimation Error (percent) | years of record | Minimum | Maximum | | |
| M1D10Y | 0.36 | 130 | | | | |
| M7D10Y | 0.5 | 130 | | | | |

| M7D2Y | 0.71 | 75 | |
|--------|------|----|--|
| M30D5Y | 0.84 | 83 | |

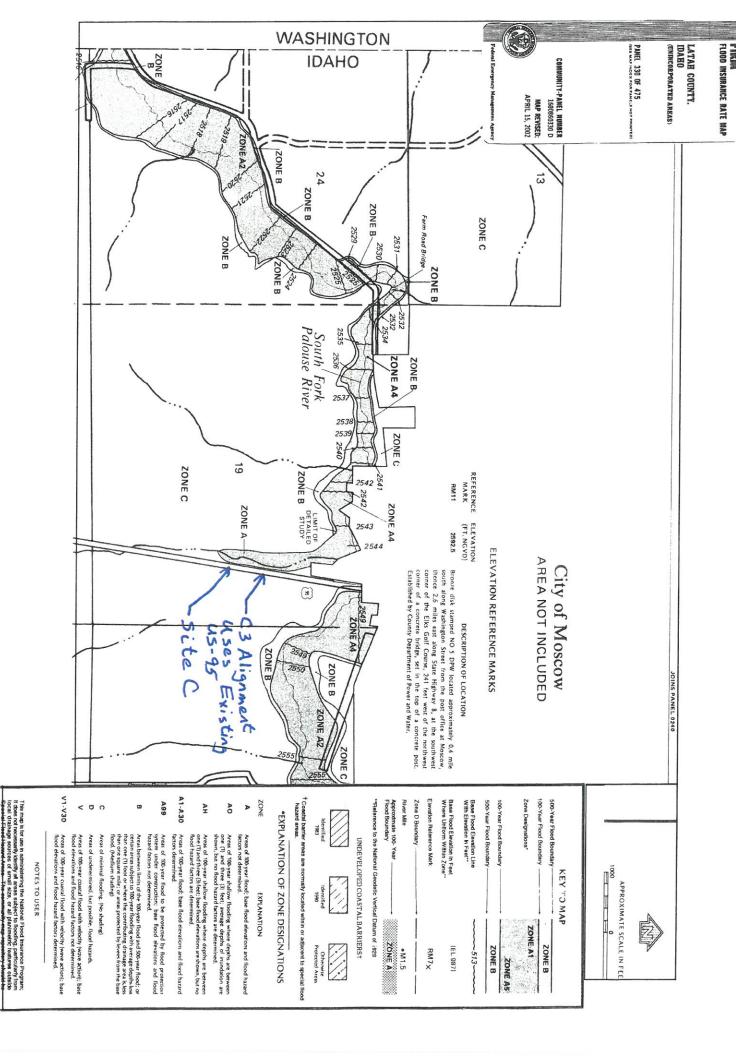
| | | | Equivalent | 90-Percent Prediction Inter | | |
|-----------|----------------------------|----------------------------|--------------------|-----------------------------|---------|--|
| Statistic | Flow (ft ⁻³ /s) | Estimation Error (percent) | years of record | Minimum | Maximum | |
| QA | 10.8 | 17 | | | | |
| JAND20 | 21.3 | 46 | | | | |
| JAND50 | 6.65 | 43 | | | | |
| JAND80 | 2.05 | 21 | | | | |
| FEBD20 | 39.5 | 39 | | | | |
| FEBD50 | 14.5 | 19 | | | | |
| FEBD80 | 5.02 | 27 | | | | |
| MARD20 | 40.5 | 41 | | | | |
| MARD50 | 19.3 | 26 | | | | |
| MARD80 | 6.9 | 26 | | | | |
| APRD20 | 19.2 | 44 | | | | |
| APRD50 | 8.74 | 46 | | | | |
| APRD80 | 4.18 | 62 | | | | |
| MAYD20 | 8.3 | 61 | | | | |
| MAYD50 | 3.85 | 51 | | | | |
| MAYD80 | 2.37 | 44 | | | | |
| UND20 | 4.01 | 43 | | | | |
| UND50 | 2.55 | 30 | | | | |
| UND80 | 1.89 | 36 | | | | |
| ULD20 | 2.06 | 21 | | | | |
| ULD50 | 1.83 | 30 | | | | |
| ULD80 | 1.73 | 50 | | | | |
| UGD20 | 1.84 | 28 | | | | |
| UGD50 | 1.78 | 44 | | | | |
| UGD80 | 1.73 | 96 | | | | |
| EPD20 | 1.88 | 22 | | | | |
| EPD50 | 1.78 | 33 | | | | |
| EPD80 | 1.72 | 63 | | | | |
| CTD20 | 1.94 | 26 | | | | |
| CTD50 | 1.83 | 25 | | | | |
| CTD80 | 1.73 | 37 | | | | |
| OVD20 | 3.21 | 67 | | | | |
| OVD50 | 1.8 | 29 | | | | |
| OVD80 | 1.77 | 28 | | | | |
| CD20 | 7.26 | 49 | | | | |
| CD50 | 1.85 | 42 | | | | |
| CD80 | 1.81 | 22 | | | | |

StreamStats Print Page

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NATIONAL FLOOD INSURANCE PROGRAM

PROJECT NO. DHP-NH-4110(156)

FLOOD PLAIN PHOTOS

ALIGNMENT C-3

SITE C

Approximate Beginning of Longitudinal

Flood Plain Encroachment of Site C

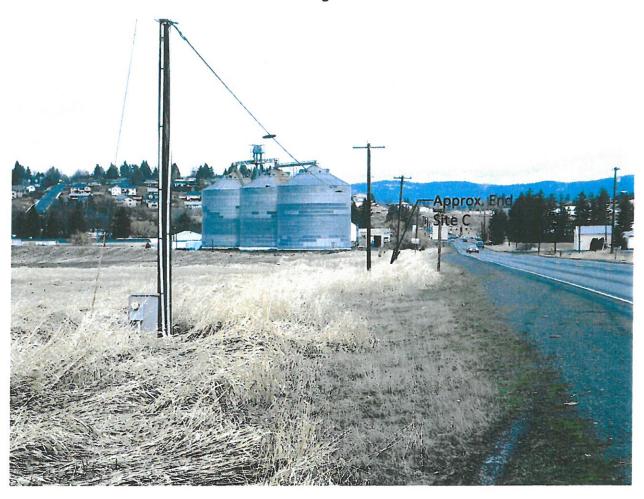
Looking South



Approximate Ending of Longitudinal

Flood Plain Encroachment of Site C

Looking North



Appendix D SOUTHEAST MOSCOW INDUSTRIAL PARK EXISTING CONDITION HYDRAULIC MODEL



MEMORANDUM #4

To:

Bill Belknap, City of Moscow

From:

Andy Heitmann, TerraGraphics, Moscow

Susan Firor, TerraGraphics, Moscow

Date:

February 22, 2010

Project Code: 09216

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Introduction

The purpose of this memorandum is to summarize the development of an existing condition hydraulic model on the South Fork Palouse River (South Fork) near Moscow, Idaho. Specifically, the memorandum will discuss the hydrologic analysis, updated model geometric data, and model results. The purpose of this investigation was to determine the accuracy of the Federal Emergency Management Agency (FEMA) Effective Flood Insurance Study (FIS) and Flood Insurance Rate Map (FIRM) by using recent topographic survey data to update FEMA's hydraulic model. The Effective FIS, FIRM, and hydraulic model have an original effective date of August 15, 1980. TerraGraphics converted the Effective model to the now-preferred modeling platform, HEC-RAS, as described in Memorandum #3, Southeast Moscow Industrial Park HEC-2 Duplicate Model. In this exercise, the converted model was updated to reflect current geometric and hydrologic data.

Subject: Southeast Moscow Industrial Park Existing Condition Hydraulic Model

Updated Geometry Data

The most significant change in the geometry data was the replacement of all the previous model cross-sections with survey data collected by TerraGraphics in 2010, as described in Memorandum #2, Southeast Moscow Industrial Park Field Survey Summary. Since the Effective hydraulic model was developed for the South Fork in 1980 the stream crossings at Highway 95 and Paradise Ridge Road have been replaced or modified. Therefore, all associated bridge data were updated in the model to reflect the current conditions. Blocked areas (obstructions) were added where cross-sections intersect buildings. During survey and while comparing cross-section data between the Effective model and the current survey, several dikes where fill material has been placed within the floodplain were noted within the project reach. Since these dikes are not certified or accredited by FEMA for flood control, they were removed from the cross-section data for the majority of modeling scenarios in accordance with FEMA guidance (FEMA, 2003). Manning's n values were changed to 0.030 (cultivated field) in areas that are currently being farmed in order to accurately represent the current farming practices. The vertical datum used in this study is NAVD88 and the horizontal datum is Idaho State Plane, Zone West, NAD 83, US survey foot.

Hydrologic Analysis

In addition to the geometry changes made in the updated model, the peak flow rates used for the 100-year return interval flood were updated. The hydrology for the Effective FEMA model, like the geometry, was developed about 30 years ago. Since that time, the United States Geological Survey (USGS) has gathered additional data for the streams in this region, and new regional regression equations were developed in 2002 (Berenbrock, 2002). Comparable regional regression analyses were completed based on the flow change locations in the effective FEMA HEC-2 model. Table 1 shows the 100-year peak flow rates for both the effective FIS model and the updated regional regression analysis.

Table 1. 100-year Peak Flow Rates for Effective and Updated Hydraulic Model.

| FIS | River | 100-year Pea | ak Flow Rates (cfs) |
|-------------|---------|----------------------|---------------------|
| Designation | Station | Effective FIS | Regional Regression |
| BB | 10334 | 1800 | 1280 |
| AV | 7150 | 1890 | 1310 |
| AP | 3746 | 2870 | 1370 |

100-year peak flow estimates at the upstream end of the US 95 Highway bridge were also acquired from the Idaho Transportation Department (ITD). Although ITD's estimate of 1080 cubic feet per second (cfs) was less than the regional regression analysis, the hydrologic analysis did not extend beyond the immediate vicinity of the bridge and, thus, was not suitable for use in this analysis.

Hydraulic Modeling Scenarios

As part of the modeling process, several different combinations of geometry and flow data were compiled into model scenarios in order to gather further insight into the current conditions and possible changes due to FEMA regulations, and to perform sensitivity analyses. Table 2 outlines the different geometry files developed with their corresponding descriptions. Table 3 summarizes the different steady flow files used in this study. Table 4 depicts the resulting model scenarios used for the existing condition modeling effort. Each model scenario uses a combination of a geometry file and a flow data file. More in-depth explanations of each scenario are presented below.

Table 2. Geometry Files Developed for Existing Hydraulic Model

| Name (short) | HEC-RAS File Name | Description |
|--------------------|-------------------|--|
| Existing | Existing | Compiled using TerraGraphics survey completed in 2010 |
| FEMA Existing_FEMA | | Same as Existing with dikes and fill removed from floodplain |

Table 3. Steady Flow Data Files Developed for Existing Hydraulic Model

| Table 3. Steady 1 low Data I hes Developed for Existing Hydraune Would | | | |
|--|---------------------------------|--|--|
| Name (short) | HEC-RAS File Name | Description | |
| FIS | FEMA HEC2 Dup | Flow data used based on effective FIS for Latah County | |
| RR | Existing_Regional Regression | Flow data based on regional regression analysis published by USGS in 2002 (Berenbrock, 2002) | |

Table 4. Scenarios Compiled for Existing Hydraulic Model

| Scenario Name | Geometry Data | Flow Data | Analysis | |
|-----------------------------|---|-----------|---|--|
| Existing | Existing | FIS, RR | Actual flooding potential based on existing topography | |
| FEMA | Existing_FEMA | FIS | Compare FIS floodplain with existing conditions using old hydrology | |
| FEMA - with Ineff | FEMA - with Ineff FIS Check for impacts of ineffe areas | | Check for impacts of ineffective flow areas | |
| Regional Regression | Existing_FEMA | RR | Compare FIS floodplain with existing conditions using updated hydrology | |
| FEMA - Floodway | Existing_FEMA | FIS | Determine Floodway extents using old hydrology | |
| RR - Floodway Existing_FEMA | | RR | Determine Floodway extents using updated hydrology | |

The Existing scenario uses the survey data collected by TerraGraphics in 2010 and represents the actual conditions currently seen along the study reach of the South Fork. The results of this scenario, although generally reflective of reality, are not applicable to this analysis because FEMA will not recognize the dikes along the South Fork unless considerable effort is made to certify them for flood control. The effort required for certification will include extensive engineering analysis, reconstruction to meet levee standards, incorporation of closure devices, and development and implementation of operations and maintenance plans (FEMA, 2008). These steps may be considered in future analyses.

The FEMA scenario is the same as the existing condition with uncertified dikes and filled areas removed. This scenario was created in order to produce a modeling condition that would be in accordance with FEMA modeling guidance and regulations. The 100-year return interval floodplain extent from this scenario is compared to the effective FEMA floodplain in Figure 1. The remaining modeling scenarios all use the FEMA geometry data.

As part of a sensitivity analysis, the next modeling scenario (FEMA – with Ineff) incorporated ineffective flow areas into the cross-sections as appropriate. This allowed for low-lying areas away from the channel to be modeled as contributing no effective flow conveyances until a specified water surface elevation (WSE) has been reached. The results showed this had little effect on the overall extents of the floodplain, so it was not used in further analyses.

The Regional Regression scenario was developed to show results based on the most current data available for both geometry and flow rates. This plan depicts what is believed to be the most accurate and acceptable approach for developing an updated model for FEMA. The floodplain extent from this scenario is compared to the effective FEMA floodplain in Figure 1.

The final two scenarios were created in order to perform encroachment analyses for the updated information using both the FIS and regional regression hydrology. Encroachment analysis is used to determine and map floodway extents along the study reach. Figures 2 and 3 show the results for the FIS and regional regression hydrology, respectively. These analyses were based on a maximum base flood elevation (BFE) rise of one foot at any given cross-section as outlined by FEMA regulations.

Existing Condition Model Results

Upon completion of all the modeling scenarios, output results were compared to published FIS values for Latah County. Table 5 compares the BFE for the Effective FIS, FEMA, and Regional Regression modeling scenarios. All elevations have been converted to NAVD88 using the NGS published conversion of 3.6 feet for this area. Table 6 shows a comparison of floodway widths from the Effective FIS and those resulting from encroachment analyses on FEMA, and Regional Regression modeling scenarios.

Table 5. Floodway WSE for Effective FIS and Modeling Scenarios

| Cross-Section | | | Base Flood Elevation (ft) | | | |
|--------------------|--------|------------------|---------------------------|----------|---------------------------------------|--|
| FIS Designation | Number | River Station | Effective FIS (1) | FEMA (2) | Regional Regression ⁽³⁾ | |
| BB | 63 | 10334 | 2563.1 | 2562.9 | 2562.4 | |
| BA | 62 | 9614 | 2561.9 | 2561.8 | 2561.4 | |
| AZ | 61 | 9038 | 2561.2 | 2561.0 | 2560.3 | |
| AY | 60 | 8306 | 2559.8 | 2560.8 | 2559.9 | |
| AX | 59 | 7890 | 2559.5 | 2560.8 | 2558.1 | |
| AW | 58 | 7808 | 2559 | 2558.6 | 2557.9 | |
| AV | 56 | 7150 | 2558.2 | 2557.3 | 2556.9 | |
| AU | 55 | 6649 | 2556.5 | 2556.5 | 2556.1 | |
| AT | 54 | 6040 | 2555.1 | 2554.4 | 2554.4 | |
| AS | 53 | 5202 | 2552.8 | 2554.3 | 2552.7 | |
| AR | 52 | 4530 | 2552.7 | 2554.2 | 2552.5 | |
| AQ | 51 | 4200 | 2552.6 | 2554.2 | 2552.3 | |
| AP | 50 | 3746 | 2552.6 | 2554.1 | 2551.7 | |
| AO | 48 | 3506 | 2552.2 | 2554.0 | 2551.2 | |
| AN | 47 | 3360 | 2550.6 | 2552.2 | 2550.7 | |
| AM | 46 | 3014 | 2549.4 | 2551.6 | 2550.2 | |
| AL | 45 | 2717 | 2548.6 | 2550.5 | 2548.7 | |
| AK | 44 | 2614 | 2548.4 | 2548.9 | 2548.2 | |
| AJ | 43 | 2411 | 2548.1 | 2548.5 | 2547.7 | |
| Al | 42 | 2287 | 2547.2 | 2548.0 | 2547.3 | |
| AH | 41 | 2137 | 2547 | 2547.6 | 2546.7 | |
| AG | 40 | 2045 | 2546.7 | 2547.5 | 2546.5 | |
| AF | 39 | 1390 | 2544.7 | 2546.9 | 2545.6 | |
| AE | 38 | 1274 | 2545.5 | 2546.8 | 2545.5 | |
| AD | 37 | 1084 | 2544.9 | 2546.6 | 2544.6 | |
| AC | 36 | 1010 | 2544.9 | 2545.6 | 2543.9 | |
| AB | 35 | 619 | 2543.6 | 2544.0 | 2542.4 | |
| AA | 34 | 107 | 2541.4 | 2543.3 | 2541.8 | |

¹ Elevation converted to NAVD88 using a 3.6' conversion factor

² Existing-FEMA geometry file and FIS hydrology

³ Existing-FEMA geometry file and RR hydrology

Table 6. Floodway Widths for Effective FIS and Existing Condition Model Scenarios

| Cross-Section | | | Floodway Width (ft) | | | |
|--------------------|--------|------------------|---------------------|------|------------------------|--|
| FIS Designation | Number | River Station | Effective FIS | FEMA | Regional Regression | |
| BB | 63 | 10334 | 77 | 95 | 38 | |
| BA | 62 | 9614 | 130 | 130 | 75 | |
| AZ | 61 | 9038 | 197 | 162 | 70 | |
| AY | 60 | 8306 | 203 | 231 | 140 | |
| AX | 59 | 7890 | 326 | 141 | 160 | |
| AW | 58 | 7808 | 254 | 141 | 141 | |
| AV | 56 | 7150 | 136 | 125 | 120 | |
| AU | 55 | 6649 | 111 | 120 | 100 | |
| AT | 54 | 6040 | 258 | 200 | 70 | |
| AS | 53 | 5202 | 75 | 470 | 161 | |
| AR | 52 | 4530 | 574 | 300 | 235 | |
| AQ | 51 | 4200 | 831 | 529 | 296 | |
| AP | 50 | 3746 | 743 | 386 | 321 | |
| AO | 48 | 3506 | 100 | 275 | 77 | |
| AN | 47 | 3360 | 121 | 250 | 71 | |
| AM | 46 | 3014 | 47 | 140 | 50 | |
| AL | 45 | 2717 | 102 | 76 | 52 | |
| AK | 44 | 2614 | 77 | 100 | 73 | |
| AJ | 43 | 2411 | 110 | 125 | 55 | |
| Al | 42 | 2287 | 53 | 150 | 75 | |
| AH | 41 | 2137 | 68 | 180 | 80 | |
| AG | 40 | 2045 | 79 | 199 | 107 | |
| AF | 39 | 1390 | 142 | 205 | 102 | |
| AE | 38 | 1274 | 140 | 218 | 110 | |
| AD | 37 | 1084 | 91 | 232 | 38 | |
| AC | 36 | 1010 | 70 | 95 | 60 | |
| AB | 35 | 619 | 95 | 59 | 48 | |
| AA | 34 | 107 | 61 | 115 | 75 | |

The modeling scenarios in HEC-RAS are based on surveyed cross-sections, so model results are given at points that fall along the cross-section lines. To display floodplain and floodway boundaries that follow the existing ground, a digital elevation model (DEM) provided by the City of Moscow was used to interpolate along the contour lines between cross-sections. Using this method allows for a more representative shape of the floodplain, but some uncertainty is introduced because the accuracy of the DEM is less than that of the survey data. Elevations of survey points along the cross-sections were compared with corresponding DEM elevations, and it was noted that the DEM was lower than the surveyed points by an average of 0.5 feet on the north side of the South Fork. To estimate the impact of this uncertainty on the floodplain extents, the DEM was raised by 0.5 feet and the floodplain extent was re-analyzed. As predicted, the floodplain extent was shifted towards the river channel slightly on the north side as compared to the previous scenario. This comparison is shown in Figure 4.

Conclusion

Significant changes to the floodplain and floodway boundaries have been modeled using updated topographic and hydrologic information. Most significantly, the width of the floodway is much smaller in much of the proposed Industrial Park area using the most recent data, although some existing buildings are still inside the floodway. In addition, although differences are noted between survey data and the DEM, resurvey of the area is not recommended, as the expected resulting decrease in flood width is not significant. Subsequent steps in this process will be discussed with City personnel at upcoming meetings.

References

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FEMA, 2008. Meeting the Criteria for Accrediting Levee Systems on NFIP Flood Maps, Federal Emergency Management Agency, July 2008.

cc: Tom Jones, WHPacific Laila Maqbool, WHPacific

